

Cost Effective Bridge Replacement and Rehabilitation Solutions

Todd Black – Area Manager - Structures Kim Cimarolli – Bridge Consultant



Meet the Team



Todd Black, PE Area Manager

Todd is the Area Manager for Kansas, Nebraska, Missouri & Illineibas over 19 years of experience in the construction/consulting industry. Todd has a BS in Civil Engineering from Kansas State University and a MS in Engineering Management from the University of Kansas.



Kim Cimarolli - Bridge Consultant

Kim is the Southern Illinois and Eastern Missouri Bridge Consultant for Contech Engineered Solutions. She graduated from the University of Missouri Rolla with a Bachelor of Science in Mechanical Engineering. Prior to joining Contech, Kim was an engineering consultant specializing in construction oversight and custom metal fabrication.

Todd and Kim are responsible for providing technical knowledge and consultative solution development to owners, engineers and contractors in the civil infrastructure industry.

Contech Engineered Solutions

Bridges & Structures, Stormwater Management, Pipe, Erosion Control and Retaining Walls



Clear Span Bridges

Pipe Solutions

i-Series™ Culvert

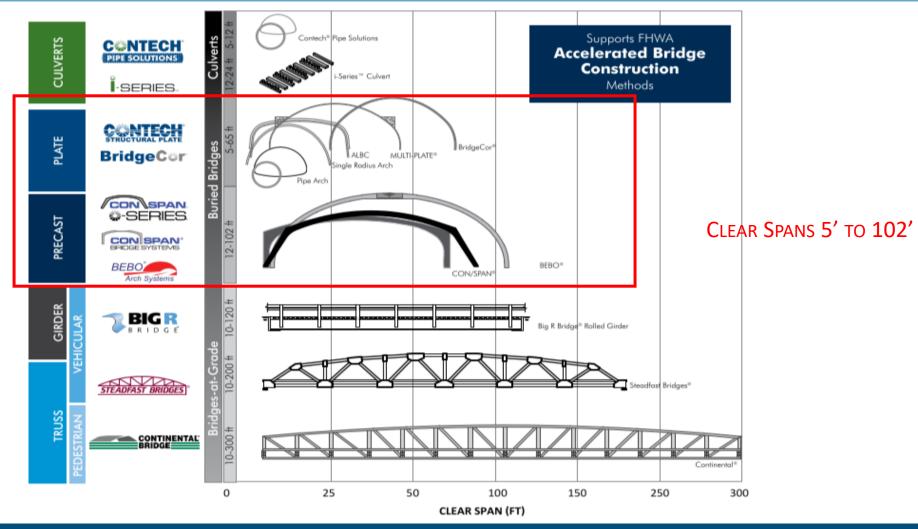
MULTI-PLATE®
Aluminum Structural Plate
Aluminum Box Culvert
SUPER-SPAN™
SUPER-PLATE®
BridgeCor®

CON/SPAN®O-Series® CON/SPAN® BEBO®

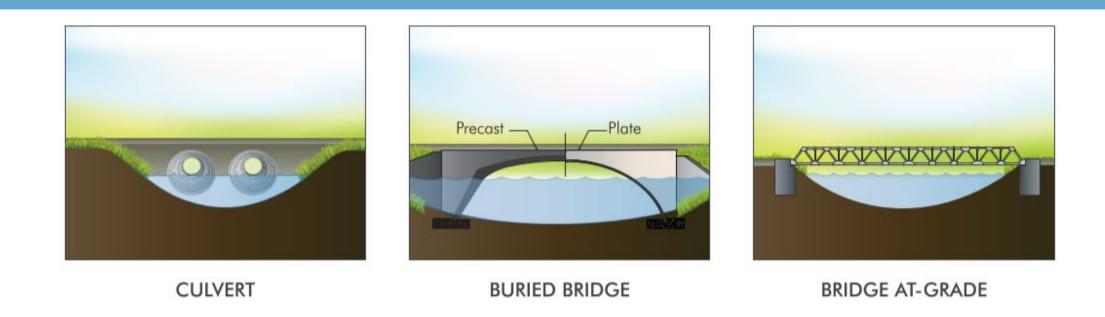
Big R Bridges® (Rolled Girder)

Steadfast Bridges®(Vehicular)

Continental®Bridges (Pedestrian)

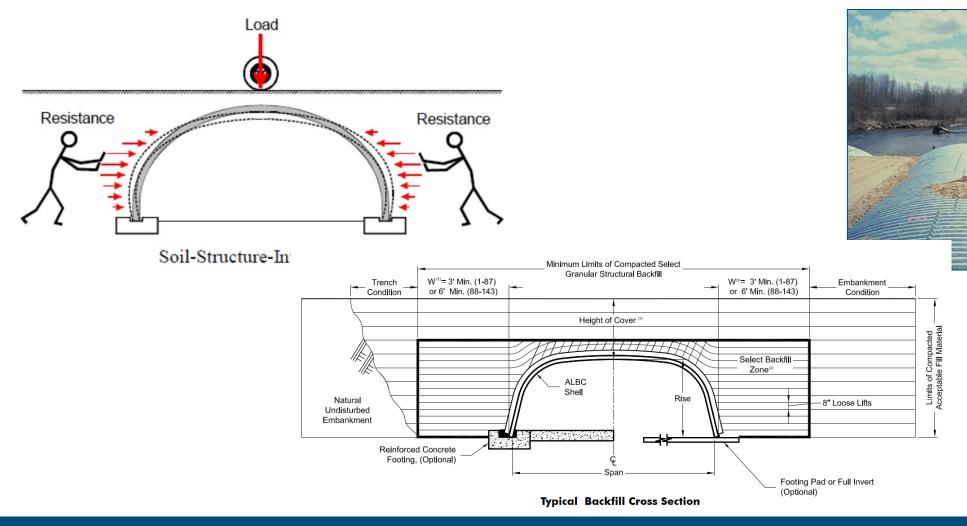


What is a Buried Bridge?



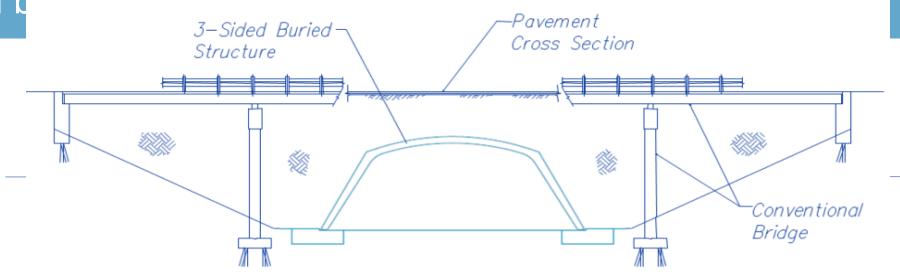
A STRUCTURE MADE OF EITHER PREFABRICATED PRECASTOR METALPLATES PLUS ENGINEERE SOIL, THATISDESIGNE AND CONSTRUCTED INDUCEA BENEFICIAL INTERACTION FTHETWO MATERIALS

Soil Structure Interaction



Buried Bridge Applications

Buried b



ADVANTAGES OF A BURIED BRIDGE OVER A BRIDGE AT GRADE

SHORTER CONSTRUCTION THE / PHASING MEANS LOWER INITIAL COST

MINIMAL / NO LONG-TERM MAINTENANCE LOWERS OVERALL LIFE CYCLE COST

- COMPARED TO CONTINUAL BRIDGE DECK MAINTENANCE
- SHORTER CONSTRUCTION TIME MINIMIZES TRAFFIC DISRUPTION
- BURY UTILITIES IN BACKFILL OVER STRUCTURE
- INCREASED SAFETY WITH LIMITED / NO FREEZE CONCERNS & DECK MAINTENANCE



Conventional

Bridge



Buried Bridge Applications

Buried bridge vs Multi - Cell Box Culvert





Buried Bridge Applications

Reline & Rehabilitation

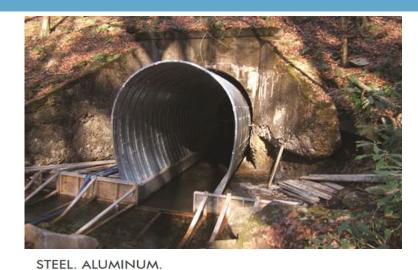


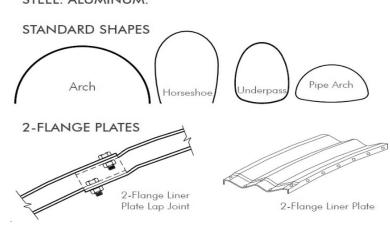


Plate









Precast

Tunnel Liner Plate



Accelerated Bridge Program



Accelera

•ABC is methods building

Prefabri

•PBES a features building construc

Connection Details for Prefabricated Bridge Elements and Systems



March 30, 2009

Publication No. FHWA-IF-09-010





HIGHWAYS FOR LIFE

Accelerating Innovation for the American Driving Experience.

C)

innovative pla anner to reduce rehabilitating

vstems

a bridge that an uction time an or replacing ex

Figure 2.4.3-1 depicts a proprietary arch system call the Con/Span® Bridge System. This system, including the arch elements, the spandrel walls, the wingwalls and the footings, can be completely made with precast concrete elements. The connections shown in Figure 2.4.3-1 are described in the following sections.

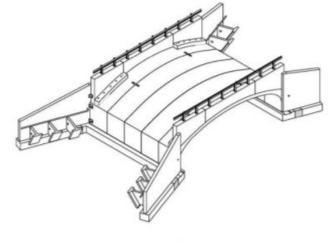


Figure 2.4.3-1 Con/Span® Bridge System

truction occurs when

id include ars when nal

"Prefabricated elements of a bridge produced offee can be assembled quickly, and can reduce design time and cost, minimize forming, minimize lane closure time and/or possibly eliminate the need for a temporary bridge."



Buried Bridge Solutions



Contech Structural Plate

In service since the 1930s

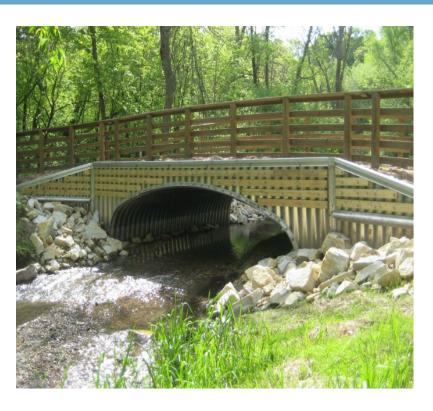




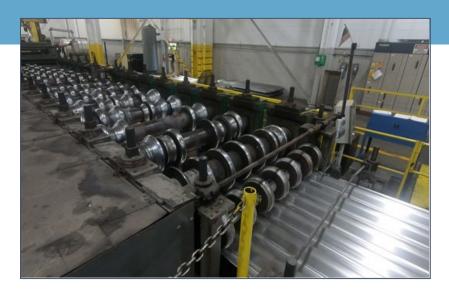


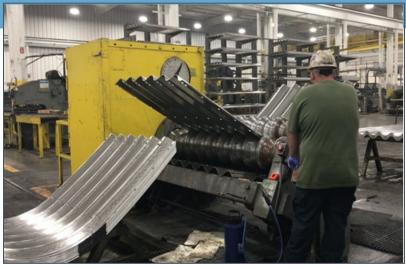






Plate Manufacturing Process















Light-weight materials for speed of construction

- Freight economy
- Reduced equipment and labor demands
- Ideal for remote site applications
- Working under utilities
- Reduced detour time









Accelerated Bridge Construction

- Preassembly reduces road closure time from weeks to days
- Prepping foundation while assembling the structure
- Structural plate can be fully or partially assembled then lifted into place
- Light weight structure may not require a crane rental
- Backfill can start immediately after installation

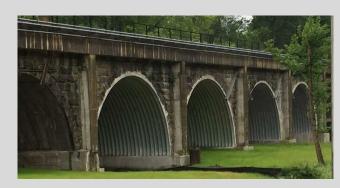




Material Options

STEEL

BRIDGECOR / MUPLATE / SUPERSPAN



Railroad Rehabilitation



ALUMINUM STRUCTURAL PLATE
ALUMINUM BOX CULVERT



Residential Development



Golf Course Community

Shape Versatility





SHAPES			STRUCTURE SIZ MULTI-PLATE* 6" x 2" Stee/	E RANGES - INSIDE SPAN 1 BridgeCor® 15' x 5.5' Steel	X RISE ALSP 9" x 2.5" Aluminum
Round		min.	5'-0' 26'-0'	19'-11" 50'-6"	6'-0' 21'-0'
Vertical Ellipse	0	min.	4'-8" x 5'-2" 25'-0" x 27'-8"		4'-8" x 5'-2" 20'-1" x 22'-3"
Underpass		min.	12'-2" x 11'-0" 20'-4" x 17'-9"		12'-1" x 11'-0" 20'-5" x 17'-9"
Single Radius Arch		min.	6'-0" x 1'-10" 26'0" x 13'1"	19'-7" x 9'-9" 54'-4" x 27'-2"	5'-0" x 1'-9" 23'-0" x 11'-11"
Two Radius Arch		min.		18'-5" x 8'-4" 50'-7" x 19'-11"	
Horizontal Ellipse		min.	7'-4" x 5'-6" 14'-11" x 11'-2"		9'-2" x 6'-8" 14'-11" x 11'-2"
Pipe Arch		min.	6'-1" x 4'-7" 20'-7" x 13'-2"		6'-7" x 5'-8" 21'-11" x 14'-11"
Low-Profile Arch SUPER-SPAN™ / SUPER-PLATE®		min.	19'-5" x 6'-9" 45'-0" x 18'-8"		19'-5' x 6'-9" 38'-8" x 15'-9"
High Profile Arch SUPER-SPAN™ / SUPER-PLATE®		min.	20'-1" x 9'-1" 35'-4" x 20'-0"		20'-1" x 9'-1" 35'-5" x 20'-0"
Horizontal Ellipse SUPER-SPAN™ / SUPER-PLATE®		min.	19'-4" x 12'-9" 37'-2" x 22'-2"		19'-4" x 12'-9" 37'-3" x 22'-2"
Pear-Arch SUPER-SPAN™		min.	23'-11" × 23'-4" 30'4" × 25'10"		
Pear SUPER-SPAN™	\bigcirc	min.	23'-8" x 25'-5" 29'-11" x 31'-3"		
Box Culvert	$\overline{}$	min.		17'-6" x 6'-10" 35'-4" x 13'-11"	8'-9" x 2'-6" 35'-3" x 13'-7"





Durability

Contributing factors of long-term durability

- pH
- Resistivity
- Hardness
- External contaminants
 - Deicing salts
 - Agricultural chemicals
- Abrasion Levels

STEEL

 $6.0 \le pH \le 10.0$ Resistivity > 2,500 ohm-cm

ALUMINUM

 $4.0 \le pH \le 9.0$ Resistivity > 500 ohm-cm







NCSPA.orgfor Service Life Calculator

• Based on CALTRANS/AISI studies of CSP

Buried bridges designed without inverts
Improves overall durability
Eliminates potential invert corrosion
Quality backfill aids in durability

Impermeable membranes over structure



End Treatments



Metal headwall



MSE Panel wall



Concrete headwall



Step-beveled end



Aluminum headwall



Wire-face basket

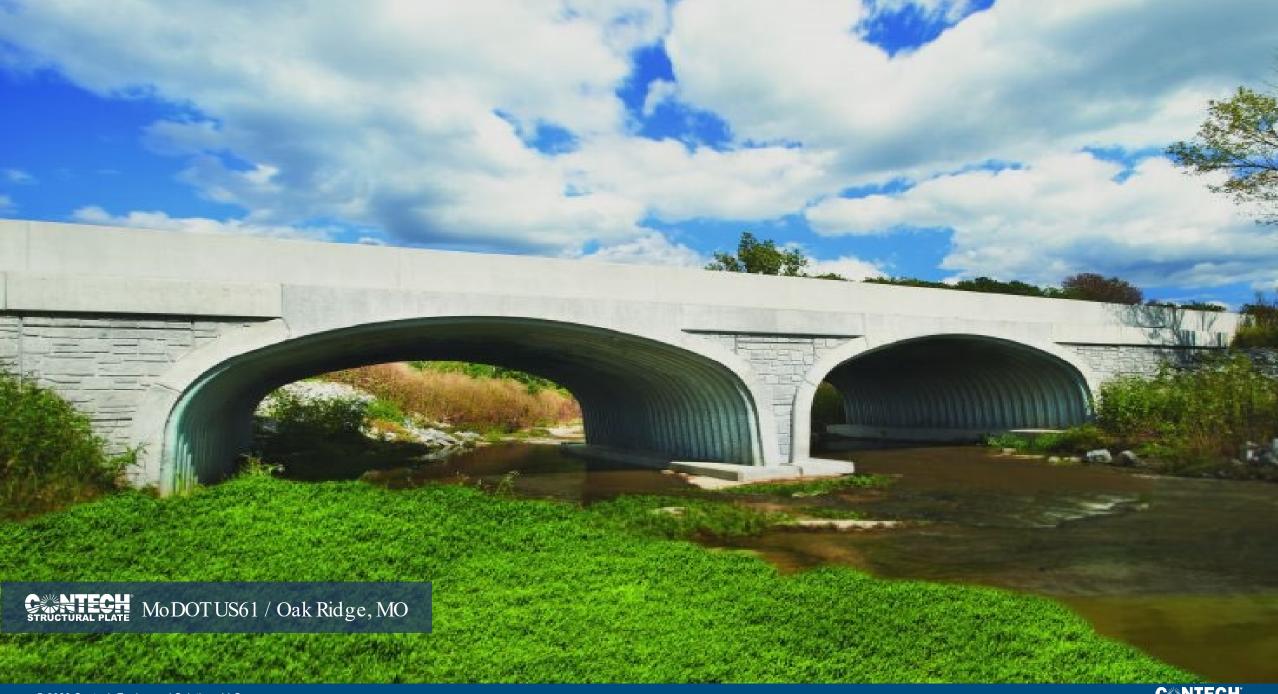




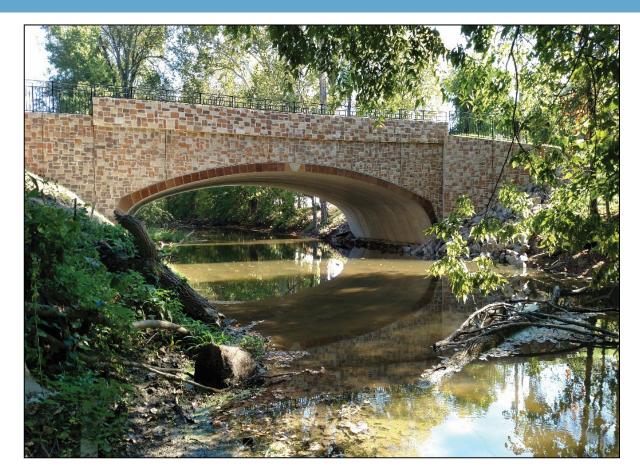




















Modular Components





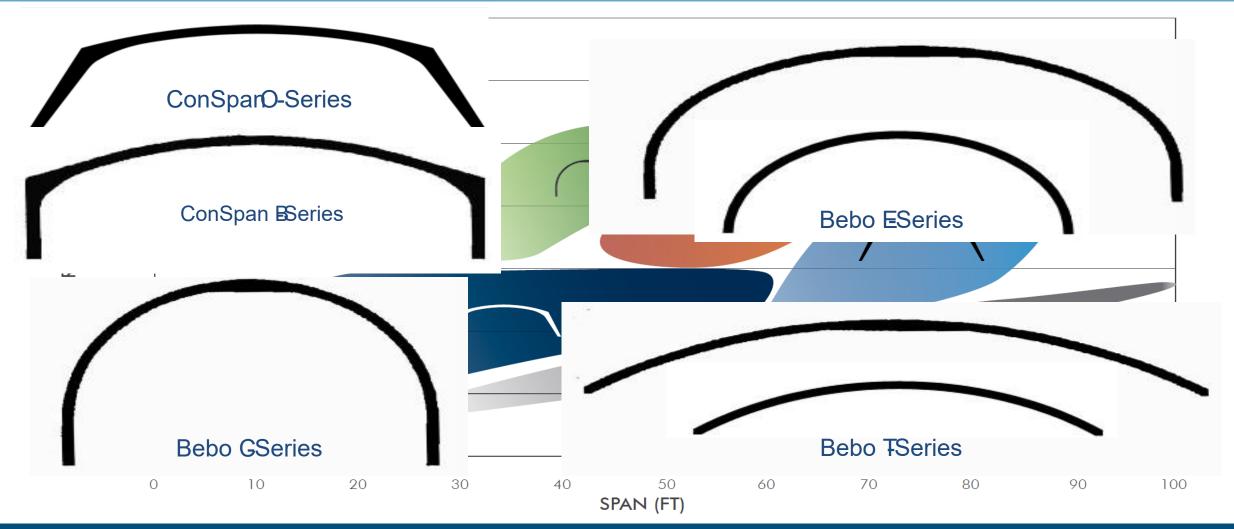








Available Shapes



End Treatments



MSE large block headwall



Precast headwall



Concrete headwall w/ formliner



MSE panel wall



Concrete headwall w/ rock face



Precast headwall w/ formliner











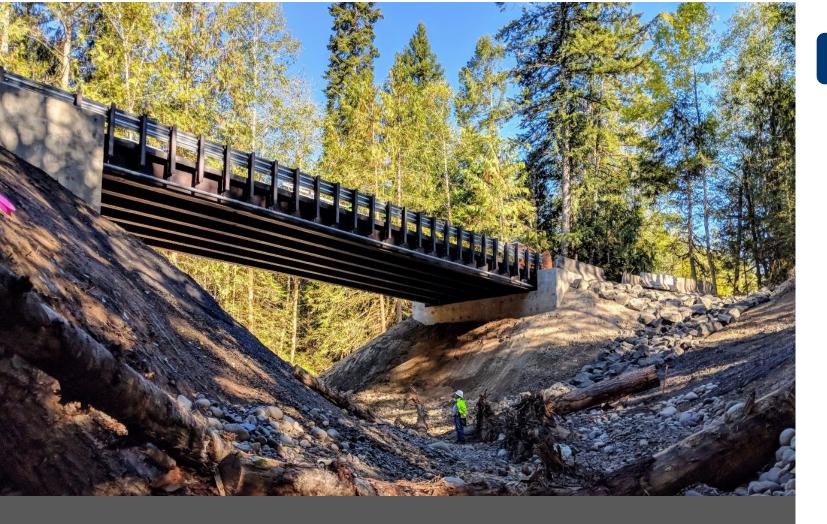






Big R Modular Rolled Girder





Modular Bridges – Accelerated Construction



Why Modular?

- Extremely cost-effective
- Ships and installs quickly
- Easy to customize
- Many rail and deck options
- •Light-weight compared to concrete
- •Great for heavy-duty vehicle loading
- Available in any width, standard single lane is 14' or 16'
- •Lengths from 10' to 140'
- A selection of Contech abutment systems
- Adaptable for use as pedestrian bridges
- AASHTO LRFD Bridge Design
 Specifications, 8th Edition, 2017

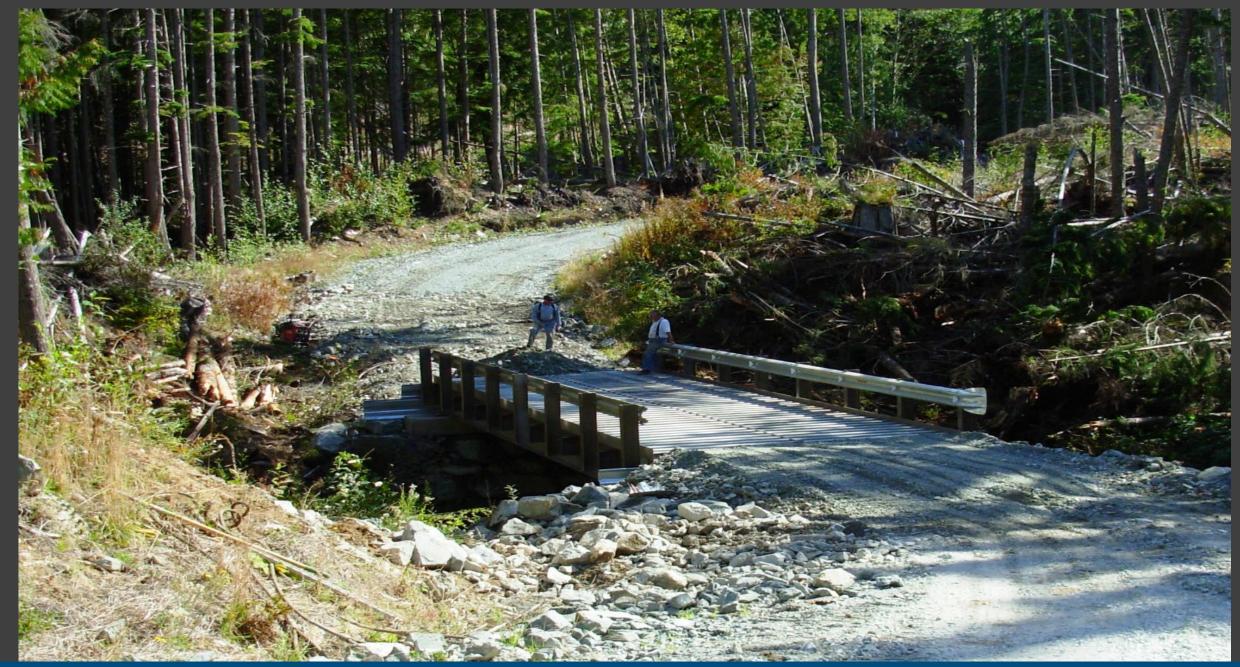


Deck Systems

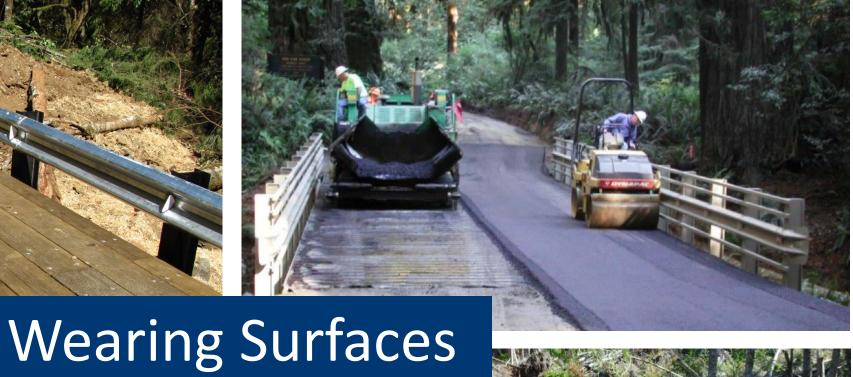










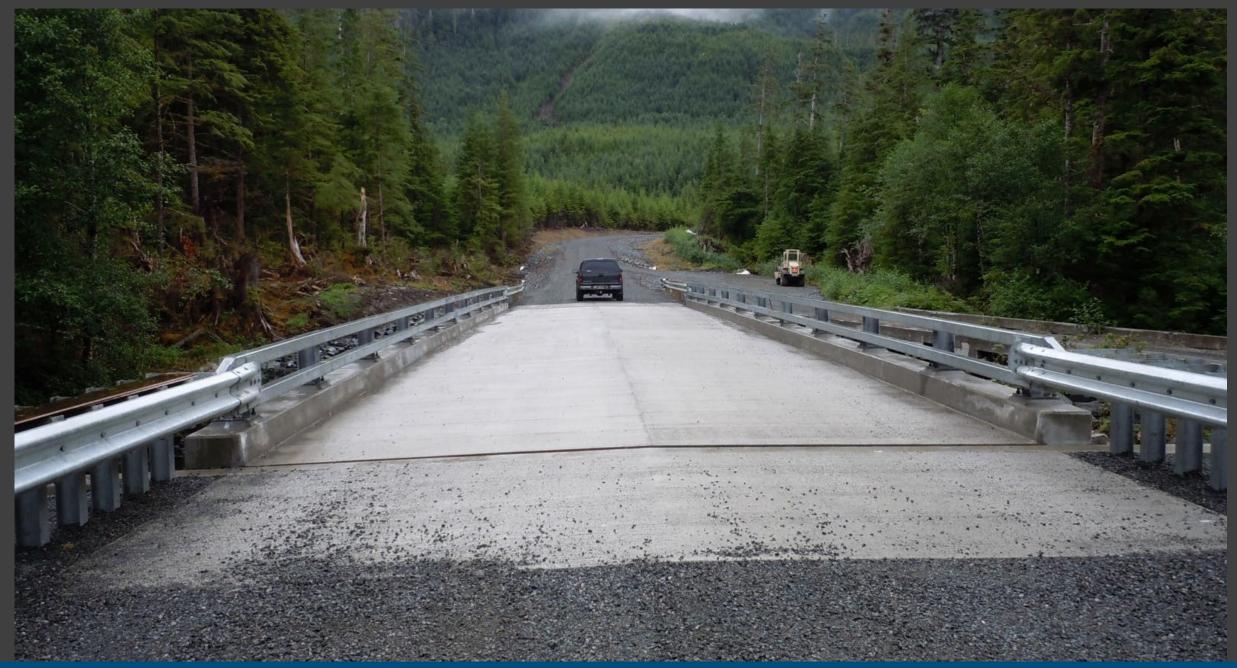












Railing Options

































RMORTEC Armortec Hard Armor Solutions













Armorflex



ArmorFlex Articulated Concrete Blocks









INVERT PROTECTION



SCOUR PROTECTION



Closed-Cell Block

DAM OVERTOPPING



Open-Cell Block

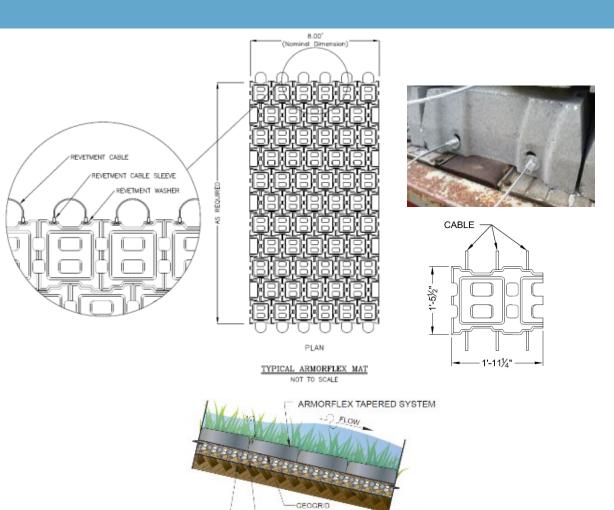
CHANNEL LINING



Block & a Half



ArmorFlex



6" MIN. DRAINAGE LAYER

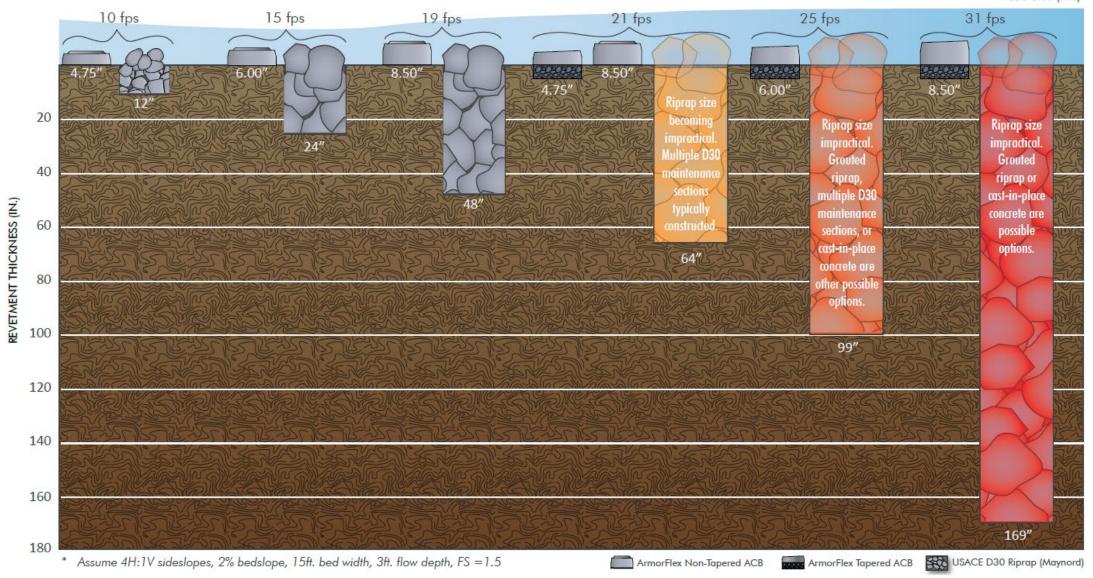
- Flexible, interlocking matrices of concrete blocks
- Uniform size, shape, and weight
- Specific Hydraulic capacities substantiated by ASTM Testing

- Mattresses or HandPlaced Blocks
 - 4 Thicknesses (4.75", 6", 7.5", 8.5")
 - 3 Footprints (0.9&f, 1.77sf, 2.5&sf)
 - 3 Types (Open, Closed, Tapered)
 - Block and a Half

GEOTEXTILE ---

ArmorFlex® ACB vs Traditional Riprap*

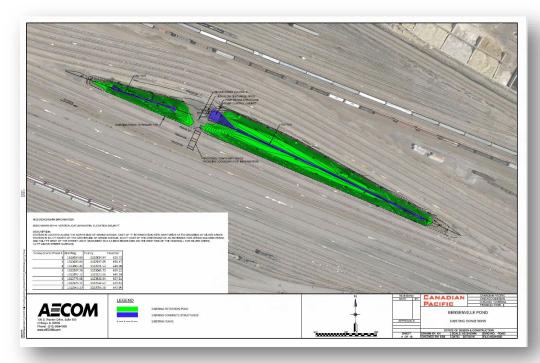
VELOCITY (FPS)





Canadian Pacific Rail Yard

Chicago, Illinois





Design Challenges

- Armoring of a stormwater detention pond
- Approximately 51,000 square feet of coverage area

Solution

• Class 45s Armorflex Closed-Cell Block

Support

- Contract drawings
- On-site installation assistance

Outcome

 Permanent, easy-toinstall and cost-effective erosion system

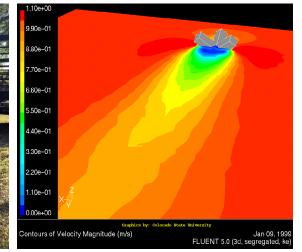




Bridge Scour – The Issues

A-Jacks Concrete Armor Units









- Interlocking, high stability armoring unit
- Palletized Sipments
- Random or uniform installation
- Hand Placed or Bundled Placement
- Rough layer (manning's n=0.1)
- Full Scale Testing
- Sizes
 - 2,4,6,8,&10





Applications





A-Jacks vs. Riprap



- Riprap
 - Assume velocity = 18 fps
 - Class VIII (1-ton) riprap 6.3' deep
 - 640 tons of riprap at 60\$/ton = \$38,400
- A-Jacks
 - Truckload (approx. 540) A-Jacks = \$17,280
 - Approx. cost to install = \$5 x 540 = \$2,700
 - Total installed cost under \$20,000



A-Jacks Installation Techniques

Typical Installation:

- 1,000 units per day
- 4-person crew
 - 1 Operator
 - 2-3 Installers
- Key is the delivery of pallets to the point of use and assembly
- Delivery of pallets with a skid-steer or telehandler works well



A-Jacks Installation Techniques





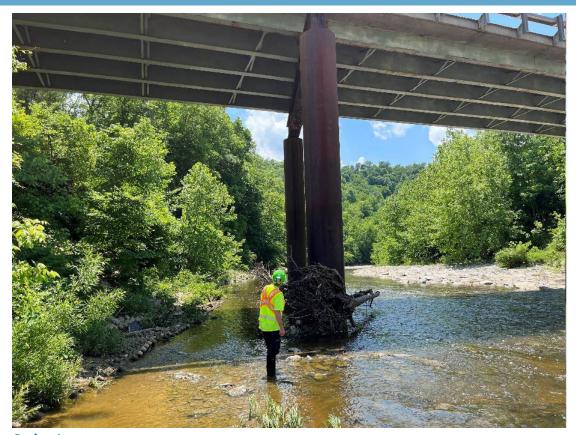
SR221 ODOT

Brown County, Ohio



Situation

- Bridge due for replacement in 5 years
- Abutments compromised due to excess bank erosion
- Needed maintenance-free solution



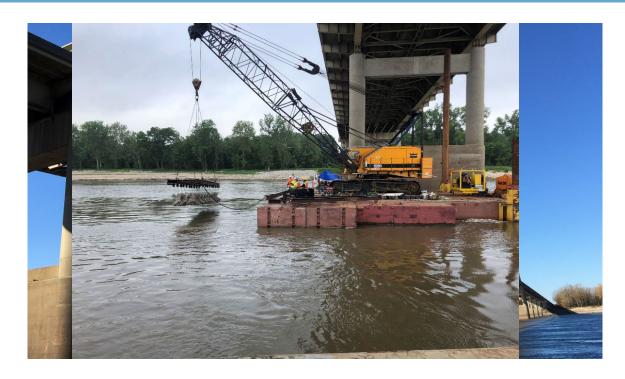
Solution

- 24" A-Jacks installed along the toe and partially up the bank
- Delayed replacement an additional 7 years beyond planned
- A-Jacks still in place, protecting new structure



TN DOT I-155 Bridge

TN / MO Mississippi River Bridge





Design Challenges

- Deep / Dangerous Water
- No Visibility
- No Ability to dewater

Solution

• 48" A-Jacks for pier scour

Support

- Specifications
- On-site installation assistance

Outcome

 Jensen Construction completed on time and on budget



Spring Creek Bridge

Ozark County, Missouri





- Erosion at toe of bridge abutment
- Labor from Department of Corrections

Solution

• 24" A-Jacks for Streambank Stabilization



Support

- Specifications
- On-site installation assistance

Outcome

 6 laborers installed system in less than 2 days





Building Blocks to a Successful Project

Solution Development

Design Support

Installation

Project Site Parameters

- Span and Rise
- Hydraulic or Clearance Box Requirements
- Environmental Compliance
- Geotechnical Data
- Type of Roadway
- Aesthetic Preferences
- Utilities
- Budget
- Schedule



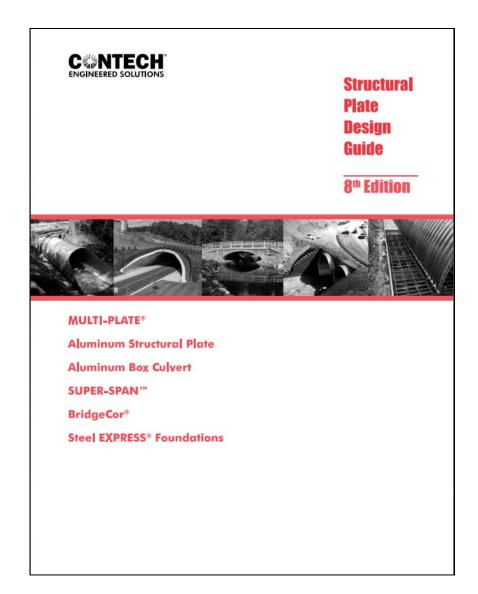




Structural Plate Design Guide

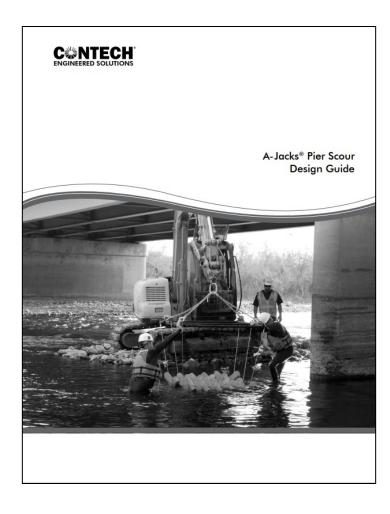
Structural Plate Technical Information

- Primary resource for structural plate
 - Design processes
 - Service life design guidance
 - Product details
 - Specifications
 - Design details for structure shapes
 - Max./min. height of cover information
 - Structure Plate make-up
 - Plate gage/thickness requirements
 - Reinforcing rib size/spacing
- NCSPA- National Corrugated Steel Pipe Association
 - Service life calculator (www.ncspa.org)





A-Jacks Design

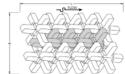


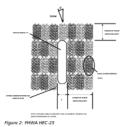
Overview

The ability of an A-Jacks matrix to dissipate energy and resist the erosive forces of flowing water allows the system to protect channel boundaries from scour and erosion Extensive laboratory testing has been performed on both model and full-scale units to determine hydraulic properties and evaluate the stability of the A-Jack units. Field tests confirmed that the A-Jacks system provides a flexible, non-erodible barrier between the channel subgrade and potentially damaging flow of water. This A-Jack Pier Scour Design Technical Note reviews the design approach as outlined in FHWA Hydraulic Engineering Circular No. 23 (HEC-23), Design Guideline 19: Concrete Armor Units. An example is included to illustrate the design procedure.

FHWA HEC-23

The design approach detailed in HEC-23 (FHWA, 2009) examines the A-Jack system in modules, also called bundles. Modules are created by banding individual A-Jacks together in a densely interlocked matrix as shown in Figure 1. Multiple module sizes can be configured and evaluated to meet project specific needs by varying the length (L) and width (B) as defined and illustrated in Figure 1 where L is





Placement

Placement of the A-Jack modules around piers is best accomplished using a rectangular pattern as illustrated in Figure 2. Orientation of the modules is recommended to be with the long dimension of the module parallel to the flow whereby providing the module a greater resisting moment. Embedment of the units will also provide greater stability since the exposed height (H_a), as defined in Figure 3, of the unit is smaller further reducing the overturning moment.

Hydraulic Stability

Hydraulic stability of an A-Jack module is estimated by setting the overturning moment, imparted by drag. equal to the resisting moment, a function of submerged weight (WS) and specific gravity (SG) of the module as illustrated in Figure 3 and defined in Equation 1. The drag coefficient (Cd) of 1.05 has been confirmed through physical hydraulic testing (FHWA, 2009).

 $F_a H_a = W_a (I/2)$ (EQ.1)

$$F_g = 0.5 C_g \rho A_g v^2$$

$$A_j = B \times H_g$$

$$W_s = W \times ([SG - 1]) SG)$$
 odultor of Gravity - To the second of the se

Table 1 can be used to create custom module sizes to accommodate specific project needs. The dimensions for length and width can be designed using the Center-to-Center Spacing, S, and the ΔX dimension as defined in Equation 2 and shown in Table 1 and Figure 3.

Table 1: HEC-23 A-Jacks Parameters

A-Jacks	Typical A-Jacks	Drag Coefficient.	Center to		ΔX
System	Weight	Coefficient,	Center Spacing, S	H _d (ft)	(ft)
	(lbs)	-4	(ft)		
AJ-24	73.6	1.05	0.75	1.3	0.66
AJ-48	590.7		1.5	2.67	1.35

L or B = $[(# \text{ of A-Jacks}) - 1] \times S + (2 \times \Delta X)$ (EO. 2)

Bedding design considerations include incorporation of a stone bedding layer, geotextile, or both. When bedding stone is used as a filter, it must meet average size and gradation requirements to retain the native bed material. Requirements are given in HEC-23 to ensure that the stone will retain the bed material, dissipate excess pore water pressure, and be large enough to resist being removed through the legs of the A-Jacks. In some cases, multiple layers of stone may be required in order to satisfy all the criteria. A suitable geotextile may be placed directly on the channel bed with A-Jack modules placed atop the geotextile, thus eliminating the need for stone bedding. n strong currents a viable construction technique is to attach the geotextile to the bottom of the A-Jack modules. Design procedures for selecting a geotextile are provided in

Design Example

FHWA HEC-23, Design Guideline 16.

A bridge crosses a 75-ft wide river where extensive scour has occurred at the bridge piers. The stream bed is 20ft below the water surface and the unstream velocity is 16-ft/s. The calculated scour depth for the 100-vr flow is 12-ft. Select an appropriate A-Jack unit size for the project conditions.

1. Calculate the Drag Force using a 4x3x4 module of 48" A-Jacks. $F_d = 0.5C_d \rho Av^2$ ρ = 1.94 slugs/ft³ $A = B \times H$ A = [((3-1) x 1.5) + (2 x 1.35)] x 2.67 A = 5.7 x 2.67 = 15.22 ft² v = 16 ft/s

2. Calculate the Overturning Moment. F_d H_d = Overturning Moment

F, H, = 10,569 lb-ft

F_a = 3,963 lbs

3. Calculate the Resisting Moment W, (L/2) = Resisting Moment

W = 11 units x 590.7 lbs = 6,498 lbs W = 6.498x ((2.083-1)/2.083)

W = 3,379 lbs $1/2 = 3.6 \, \text{FT}$ $W_{-}(L/2) = 12.163 \text{ lb-ft}$ 4. Compare the Overturning and Resisting Moments F_d H_d < W_s L_w 10,569 lb-ft < 12,163 lb-ft

The 4x3x4 48" A-Jack module has sufficient capacity to resist the overturning moment.

5. Evaluate a 6x5x6 module of 24" A-Jacks.

```
a. Calculate the Drag Force.
     F_{_{d}}\,=0.5C_{_{d}}\,\rho Av^2
            C<sub>d</sub> = 1.05
             ρ = 1.94 slugs/ft<sup>3</sup>
             A = B x H
            A = [((3-1) \times 0.75) + (2 \times 0.66)] \times 1.3
            A = 2.82 x 1.3 = 3.7 ft<sup>2</sup>
               = 16FT/s
     F<sub>d</sub> = 964.7 lbs
```

b. Calculate the Overturning Moment F_d H_d = Overturning Moment

H_d= 1.3 ft F_d H_d = 1,254 lb-ft

c Calculate Resisting Moment

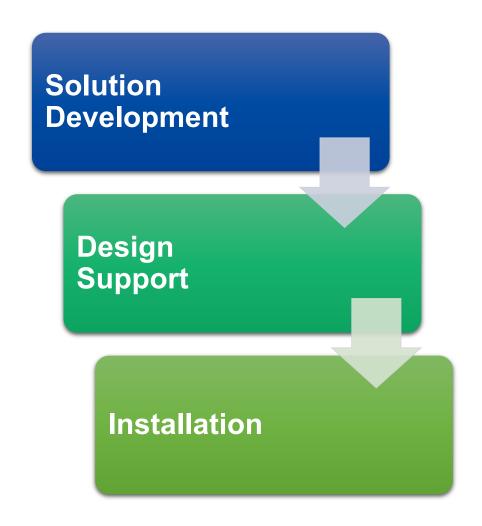
W. (L/2) = Resisting Moment W = 17 units x 73.6 lbs = 1,251 lbs W₁ = 1,251 x ((2.083-1)/2.083) W, = 650.5 lbs $1/2 = 2.54 \, \text{ft}$ $W_{L}(L/2) = 1,649 \text{ lb-ft}$

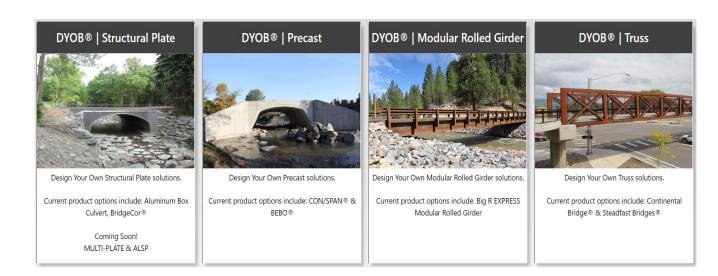
d. Compare the Overturning and Resisting Moments.

F_d H_d < W_s L_w 1.254 lb-ft < 1.649 lb-ft

The 6x5x6 24" A-Jack module has sufficient capacity to resist the overturning moment and therefore is also a viable design alternative.

Building Blocks to a Successful Project







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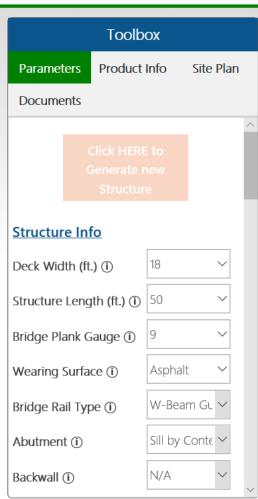


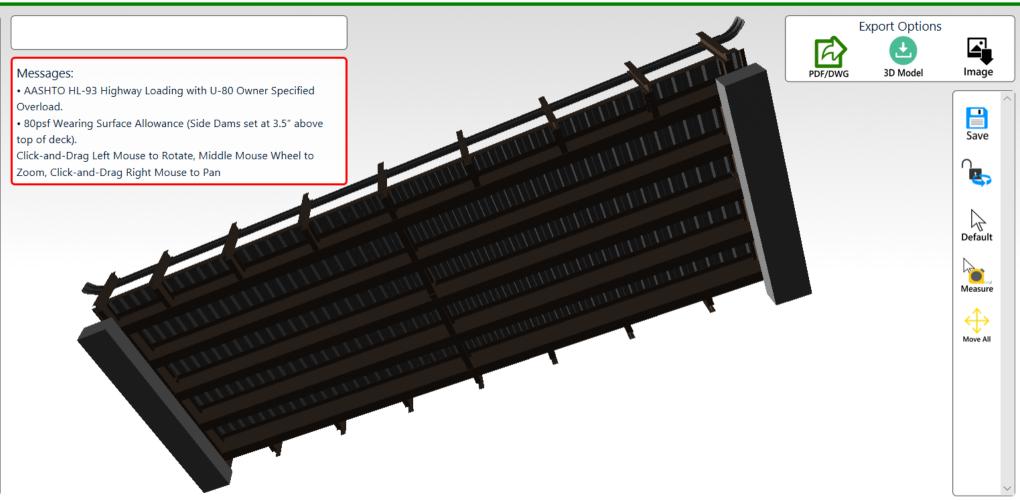


Big R Test

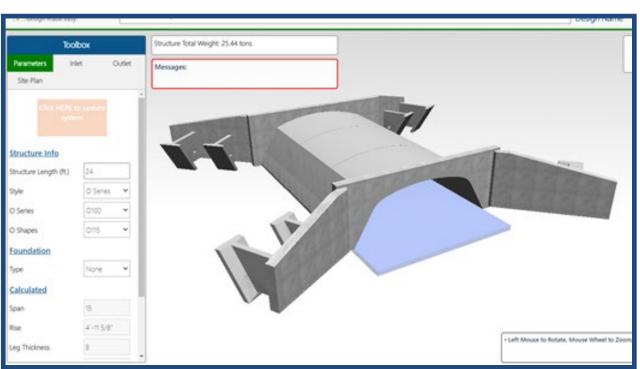
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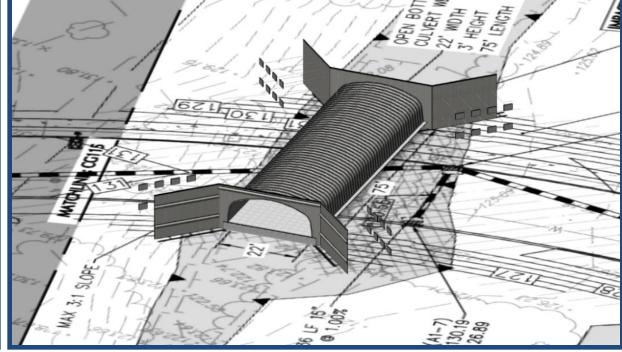
My Projects



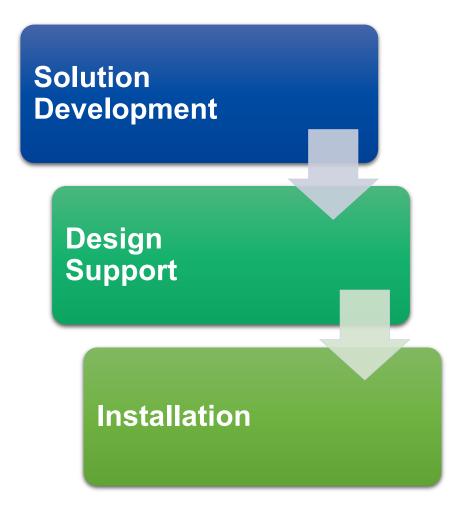


CINTECH® DESIGNCENTER





Building Blocks to a Successful Project



- Scope Letters and Installation Guides
- Attending Pre-Bid Meetings









- Preconstruction Meetings
- Onsite Technical Support Available (Field Consultant on all Precast Installations)



Contech. Your project partner.

- One-on-one Project Consultation
- More in-depth, technical information for a specific product or solution
- Schedule a presentation series, covering tailored topics each month
- Help with tools such as DYOB (Design Center) and Structural Plate Design Guide
- Provide preliminary estimates
- Assist with plans and specifications

Options & Support

Specific to Your Project Needs

Kimberly.Cimarolli@ContechES.com

314-807-3023

