

The Science You Build On.

FINANCIAL AND SCHEDULE BENEFITS OF PROJECT-SPECIFIC LOAD TESTING

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Introduction

- Foundation design process
- I-35W Bridge Replacement
- TH 610
- Conclusions

Foundation Design Process – Idealized!

- Structure need identified
- Preliminary structure design
- Subsurface exploration
 - Design-phase load test
- Final design
- Construction
 - Construction-phase load test

Project Locations



(©Google Earth 2016, 2018; MnDOT 2016)

I-35W Bridge – Collapse



I-35W Bridge – Collapse



I-35W Bridge – Design

- Twin bridge replacement
- 125-year design life
- Overall length of 1,223 feet (373 m)
- Combined width of 176 feet (54 m)
- Foundation
 - Driven H-piles
 - Drilled shafts



I-35W Bridge – Design



I-35W Bridge – Design



I-35W Bridge – Subsurface Conditions

- Primarily bedrock
- Artesian conditions
- Environmental challenges from previous development



I-35W Bridge – Preliminary Shaft Design

- Rock Quality Designation (RQD) varied from 0% to 97%
- Unconfined compressive strength varied from 40 to 2,100 psi

	Geotechnical Unit Resistance (ksf)				
	Side Shear	End Bearing	Diameter (inches)		
2 and 3	0 E to 10	60 to 150	84		
4	0.5 to 10	60 (0 150	96		

I-35W Bridge – Load Test

- Test and method shaft at Pier 3
- 78-inch-diameter, 39foot-long, rock socket





I-35W Bridge – Load Test

- Two-level, three-stage, bidirectional load test
 - 1. Upper assembly closed, lower assembly pressurized
 - 2. Upper assembly pressurized, lower assembly open
 - 3. Upper assembly pressurized, lower assembly closed



I-35W Bridge – Load Test



I-35W Bridge – Unit Resistance Summary

	Nominal Unit Resistance (ksf)			
Design Stage	Side Shear	End Bearing		
Initial	0.5 to 10 ksf	60 to 150 ksf		
Test Shaft Design	2 to 8 ksf	150 ksf		
Final (Test Shaft Actual)	2 to 40 ksf	90 ksf		

- 400 to 2,500 percent increase in side shear resistance for more-competent sandstone
- End bearing resistance agrees with design estimates

I-35W Bridge – Final Shaft Design

	Pier 2	Pier 3	Pier 4
Initial Design Diameter (inches)	84	84	96
Final Design Diameter (inches)	78	90	90
Initial Design Socket Length (feet), overall / more-competent	136 / 68	124 / 41	215 / 171
Actual Socket Length (feet), overall / more-competent	54 / 22	50 / 23	80 / 16

I-35W Bridge – Final Shaft Design

Lesscompetent sandstone





Morecompetent sandstone





I-35W Bridge – Cost Comparison

- Drilling cost of \$45 per cubic foot in both soil and rock
- Cost of initial design: \$15,162,976
- Cost of final design:
 - Testing: \$583,000
 - Construction: \$7,726,612
 - Total: \$8,309,612
- Net savings resulting from testing: \$6,853,364

I-35W Bridge – Foundation Support Cost



 Testing resulted in total support cost savings of \$17.81 per utilized kip of support

I-35W Bridge – Time Savings

- Initial design length (3,114 ft) actual length (836 ft) = 2,278 feet of less drilling in more-competent rock
- Observed drilling rate of 1 to 4 feet/hour in more-competent rock means initial design would have required an additional 570 to 2,278 hours (23 to 95 days) of drilling

TH 610 Design



TH 610 – Subsurface Conditions



TH 610 – Foundation Design

		Blow	Friction				
Soil		Count,	Angle, f	Cohesion, c			
Туре	Consistency	N ₆₀ (bpf)	(deg.)	(psf)	β	N _t	
Lean Clay (CL [*])	Soft	2 - 4	-	250 - 500	0.15	3	
	Firm	5 - 8	-	750 - 1,200	0.19	8	
	Stiff	9 - 15	-	1,500 - 2,500	0.20 - 0.29	14 - 19	
	Very Stiff	16 - 30	-	2,500 - 4,500	0.30 - 0.35	25 - 30	
	Hard	31 - 60	-	4,500 - 9,000	0.36 - 0.40	30 - 33	
	Very Hard	61+	-	10,000	0.41 - 0.50	37 - 40	
Poorly Graded	Very Loose	0 - 4	28 - 29	-	0.15 - 0.20	15 - 20	
	Loose	5 - 10	30 - 31	-	0.21 - 0.25	20 - 30	
	Medium	11 17	32 - 33	-	0.26 - 0.39	30 - 45	
	Dense	11 - 1/					
Sand (SP/SP- SM*)	Medium	10 24	33 - 34	-	0.40 - 0.52	45 - 60	
	Dense	10 - 24					
	Dense	25 - 30	35	-	0.53 - 0.59	60 - 75	
	Dense	31 - 50	36 - 38	-	0.60 - 0.75	75 - 120	
	Very Dense	51+	38 - 40	-	0.76 - 0.90	120 - 150	
*Classification based on ASTM D2487 (2011).							

Beta method, modified by experience

TH 610 – Pile Testing

- Closed-end pipe (CEP) piles
 - Diameter: 12 ¾-inch
 - Wall thickness: ¼-inch
- High-strain dynamic testing
 - Initial drive and restrike
 - Case method and wave matching using CAPWAP

TH 610 – Pile Testing

Test results versus prediction



- Total bias of 0.81 for initial and 1.22 for restrike
- Side resistance bias of 0.83 and 1.56

TH 610 – Length Comparison



TH 610 – Costs



TH 610 – Costs

- Total design length less installed length is 13,548 ft
- Assume \$30/ft for savings of \$406,440
- High-strain dynamic testing fee \$51,584
- Estimated total savings of \$354,856
- For average pile length, saved approximately 28 days of driving

TH 610 – What does it mean?



- High-strain dynamic testing is more accurate than static analysis – maybe
 - Experience in static models
 - Over-estimate length for bidding
- Can't compare with lengths for formula or static load test

TH 610 – Conclusions

- Empirical methods are inaccurate, even with experience
- Restrike testing results in higher nominal resistance than initial-drive testing
- Foundation support cost analysis during design won't have all the information
- Foundation support cost analysis postconstruction is also difficult with driven piles

I-35W Bridge – Summary

- Load testing cost \$1.52 per kip of utilized support
- Increased side shear resistance by 400 to 2,500 percent
- Testing saved \$17.81 per kip of utilized support and between 23 and 95 days of drilling

Both Projects – Conclusions

- Initial designs based on empirical values can be conservative
- Construction control with testing can be expensive, which can lead to easy dismissal
- Support cost provides a method of perspective



Both Projects – Conclusions



- Time-savings is important consideration that is not part of support cost
- Savings from test can be many times the total of testing cost

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FLATIRON MANSON





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Questions and Thank You!

